

IN THE CLAIMS

The claims have been amended as follows:

1. (Original) A system, especially adapted for high-power motors comprising at least one rotor (1a ; 1b) and means (4a, 4b ; 5a, 5b) comprising active elements (7, 8) capable of rotating the rotor(s) (1a ; 1b) by their synchronized deformation, said rotating means of the rotor(s) comprising at least one petal (6) comprising a hot top (11), characterized in that the material of each hot top (11) is such as that it has a mass thermal capacity (C_p^{22C}) of greater than 0.35 [J/g/K], and / or the material of each rotor (1a ; 1b) is such that it has a thermal capacity of greater than 2 [J/cm³/K].

2. (Original) The system according to Claim 1, characterized in that each hot top (11) has a mass thermal mass capacity greater than 0.5 [J/g/K].

3. (Currently Amended) The system according to Claim 1 or Claim 2~~Claims 1 or 2~~, characterized in that the thermal capacity of each rotor (1a ; 1b) is greater than 2.5 [J/cm³/K].

4. (Currently Amended) The system according to ~~Claims 1 to 3~~Claim 1, characterized in that the material of each hot top (11) and each rotor (1a ; 1b), this material being uncoated, comprised of:

(Ti, Mo) (C, N) + 8 - 20% bonding Ni/Mo (TM 8, 10, 20 grades 0; and / or

WC- 6Ni; and/or

zirconium reinforced aluminum (ZTA, ZTPA) ; and or

AlN; and/or

silicon carbide infiltrated with silicon SiSiC, with 8 - 20% by weight of silicon.

5. (Currently Amended) The system according to ~~one of Claims 1 to 4~~Claim 1, characterized in that the material of each hot top (11) is comprised of:

MgO – ZrO₂, and / or

aluminum reinforced with zirconia (ZTA, ZTPA), and / or

hot sintered aluminum nitrate HIP-AlN, and / or

pressure sintered aluminum nitrate GPS-AlN, and / or

a Magneli phase (Ti_nO_{2n-1}, 4 ≤ n ≤ 10 with n being an integer, or the 40% Ti₄O₇ / 60% Ti₅O₉ type mixtures).

6. (Currently Amended) The system according to ~~one of Claims 1 to 3~~Claim 1, characterized in that the material of each hot top (11) and each rotor (1a ; 1b) is coated by thermal spraying using a material comprising:

Magneli phases (Ti_nO_{2n-1}, 4 ≤ n ≤ 10 with n being an integer, or the 40% Ti₄O₇ / 60%

Ti₅O₉ type mixtures);

WC – 17% Co ; and / or

(Ti, Mo) (C, N) or (Ti, W) (C, N) + bonding Ni/Mo ; and / or

$>75 \text{ Cr}_3\text{C}_2 / < 15 \text{ NiCr}$; and / or

$4 - 6 \text{ Al}_2\text{O}_3 / 6 - 4 \text{ TiO}_2$.

7. (Original) The system according to Claim 6, characterized in that the material of each hot top (11) comprises:

globular gray cast iron and / or lamellar gray cast iron and / or with an austempering and / or alloyed with Cr, Mo, Al, V, Ti ; and or

Steels (z6CND16-05-01) ; and / or

X5CrNiCu15-5 steels ; and / or

AlSi + SiC/Al₂SO₃ ; and / or

AlSi + dispersoids Al₄C₃ / Al₂O₃ / TiB₂ alloys ; and or

Al - Fe - V alloys; and / or

Series 6xxx aluminum in T6 and greater and 7xxx series ; and / or

silicon carbide infiltrated with silicon SiSiC ; and / or

Titanium alloys, UNS R5xxxx, such as TiA16V4.

8. (Original) The system according to Claim 6, characterized in that the hard layers deposited by thermal spraying must be machined to the final roughness of R_a (arithmetic roughness) of less than 0.04 μm, the thickness of the machined layers being greater than 50 μm.

9. (Original) The system according to Claim 6. characterized in that the values of roughness R_{pK} and R_{vK} of the DIN NUMERIC ENTRY WORD ISO 13565 - 2 :1998 norm are less than $0.030\text{ }\mu\text{m}$. and $0.070\text{ }\mu\text{m}$, respectively.